

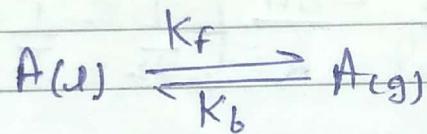
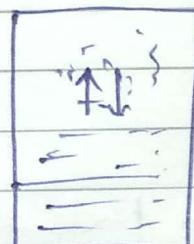
# SBG STUDY

23/09/17

## \* Liquid Solution \*

\* Pure Vapour pressure of Liquid:

If a liquid present in a close container it hold eqb. with its vapour at eqb. Pressure exerted by vapour called vapour pressure of liquid



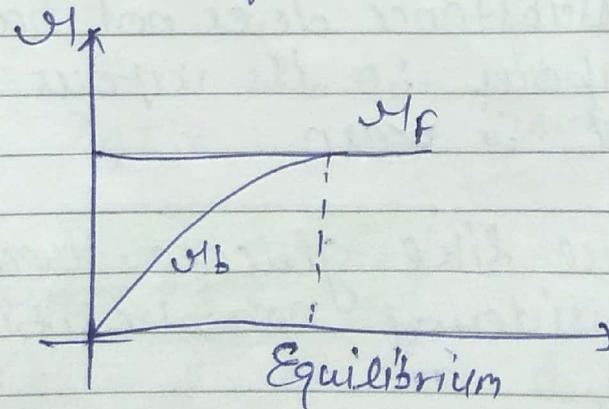
$$K_p = \frac{P_A^o}{1}$$

$$\dot{M}_F = K_F [A(l)] = K_F^*$$

$$\dot{M}_B = K_B [A(g)]$$

$\dot{M}_F$  = rate of evaporation

$\dot{M}_B$  = rate of condensation



\* Important point :

(i) Vapour pressure of pure liquid depend only on temp.  
it does not depend on ~~shape and size~~ of container.

$$P^\circ = K_{eq} = A \cdot e^{-\Delta H/RT}$$

$$\ln \left( \frac{P_2^\circ}{P_1^\circ} \right) = -\frac{\Delta H}{R} \left( \frac{1}{T_2} - \frac{1}{T_1} \right)$$

2. Intermolecular Bonding in liquid state ↓

V.P of liquid ↑

$$P_{C_6H_6(l)}^\circ > P_{H_2O(l)}^\circ$$

3) Non-volatile substance does not have a tendency to form vapour, so its vapour pressure is considered as zero

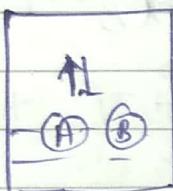
4) Solid substance like glucose, urea, sucrose, NaCl etc are considered non-volatile substance.

$$P_{\text{glucose}}^\circ = 0$$

## Raoult's law

\* Vapour pressure of liquid solution:

According to Raoult Law <sup>vapour</sup> Partial pressure of a liquid in it will be proportional to its mole fraction in liquid solution



for A

$$P_A \propto x_A$$

$$P_A = x_A P_A^{\circ}$$

for B

$$P_B \propto x_B$$

$$P_B = x_B P_B^{\circ}$$

$$P_T = P_A + P_B$$

$$P_T = n_A P_A^{\circ} + n_B P_B^{\circ}$$

Important

$P_T$  or  $P_s \Rightarrow$  v.p. of solution

$x_A$  &  $x_B$  = mol fraction of A & B in liquid phase

$$x_A = \frac{n_A}{n_A + n_B}$$

$$x_B = \frac{n_B}{n_A + n_B}$$

$$x_A + x_B = 1$$

$P_A^{\circ}$  &  $P_B^{\circ} \Rightarrow$  v.p. of pure A & pure B respectively

\* Vapour pressure of liquid solution depend on Temp. and composition of liquid solution

Graph :- ( $T = \text{const.}$ )

$$P_T = \pi_A P_A^{\circ} + \pi_B P_B^{\circ}$$

$$= \pi_A P_A^{\circ} + (1 - \pi_A) P_B^{\circ}$$

$$\pi_A P_A^{\circ} + P_B^{\circ} - P_B^{\circ} \pi_A$$

$$\pi_A (P_A^{\circ} - P_B^{\circ}) + P_B^{\circ}$$

$$P_T = \pi_A (P_A^{\circ} - P_B^{\circ}) + P_B^{\circ}$$

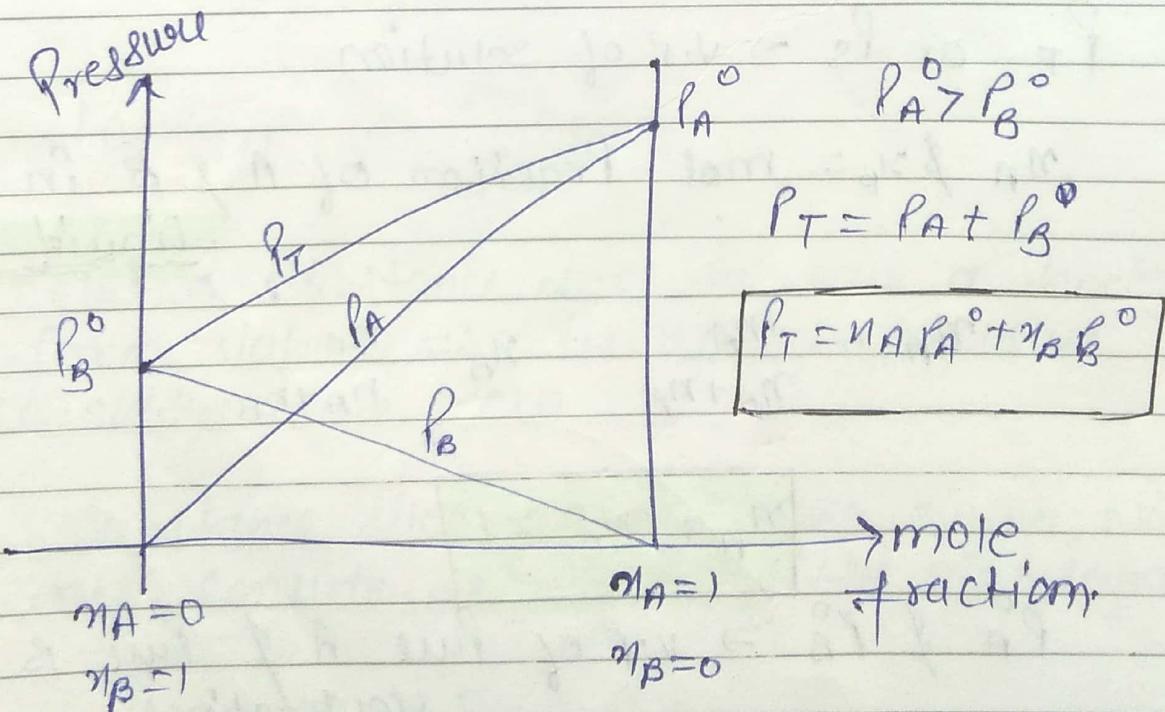
$$y = mx + c$$

$$P_A = \pi_A P_A^{\circ}$$

$$P_B = \pi_B P_B^{\circ}$$

$$P_B = (1 - \pi_A) P_B^{\circ}$$

$$P_B = -\pi_A P_B^{\circ} + P_B^{\circ}$$



Note: At boiling point Vapour pressure of liquid will be equal to external pressure and liquid hold eqb. with its vapour.

$$P_A^{\circ} > P_B^{\circ}$$

$$T_A^{\circ} < T_B^{\circ}$$

Ques. Calculate Vapour pressure of 1 molal aq. glucose solution if vapour pressure of pure  $H_2O$  is 600 Torr.

$$P_T = \pi_{H_2O} P_{H_2O}^{\circ} + \pi_{\text{glucose}} P_{\text{glucose}}^{\circ}$$

$$\Rightarrow \frac{\text{mole of Solute}}{\text{mass of Solvent in kg}} = 1$$

$$= P_T = \text{mass}$$

Let mass of solvent = 1 kg.

$$\text{mol of Solute} = 1 \\ (\text{glucose})$$

$$= \frac{n_{H_2O}}{n_{H_2O} + n_{\text{glucose}}} \cdot (600)$$

$$P_T = \frac{\left(\frac{1000}{18}\right)}{\left(\frac{1000}{18}\right) + 1} (600)$$

Q. Vapour pressure of 30% weight / Volume ag. Solution of sucrose is 400 torr if density of solution is 1.2 g/ml then calculate vapour pressure of pure  $H_2O$

$$\text{Molality} = \frac{\text{Weight}}{\text{gm}} \text{ molar mass} = 342$$

$$\text{Weight of Solute} \times 100 = 30$$

$$m = \frac{\text{Weight}}{V_{\text{solution}}}$$

Let Volume of solution is 100 ml

$$\frac{w_{\text{solute}}}{V_{\text{solut}}} \times 100 = 30$$

then weight of solute = 30 g

$$V_{\text{solut}} = 100$$

$$w_{\text{solute}} = 30$$

$$P_T = n_{H_2O} P_{H_2O}^0 + n_{\text{sucrose}} P_{\text{sucrose}}^0$$

$$P_T = n_{H_2O} P_{H_2O}^0$$

$$V = 400$$

$$D = \frac{m}{V}$$

$$m = D \times V$$

$$\text{m of solution} = 120 \text{ g.}$$

$$400 = \frac{n_{H_2O}}{n_{H_2O} + n_{\text{sucrose}}} \times P_{H_2O}^0$$

$$400 = \frac{(90/18)}{(90/18) + 30} \times P_{H_2O}^0$$

$$342$$

\* Relation b/w  $y_A$ ,  $y_B$  &  $P_T$  :-

(1) Partial Pressure of A and B can be calculated from Raoult's law from mol fraction of A and B present in liquid phase

$$P_A = n_A P_A^{\circ} \quad P_B = n_B P_B^{\circ}$$

(2) From Dalton's law of partial pressure, Partial Pressure of A and B can be calculated with the help of mole fraction of A and B present in vapour phase

$$\begin{aligned} P_V &= n' k T \\ P_T V &= n' R T \\ \frac{P_A}{P_T} &= \frac{n'_A}{n'} \\ P_A &= y_A P_T \end{aligned}$$

$$P_A = y_A P_T$$

$$P_B = y_B P_T$$

Here,  $y_A$  and  $y_B$  are mol fraction of A & B in vapour phase

\* By Comparing Raoult's law with Dalton's law

$$n_A P_A^{\circ} = y_A P_T$$

$$n_B P_B^{\circ} = y_B P_T$$

$$y_A = \frac{n_A P_A^{\circ}}{P_T}$$

$$y_B = \frac{n_B P_B^{\circ}}{P_T}$$

$$n_A + n_B = 1$$

$$\frac{y_A P_T}{P_A^{\circ}} + \frac{y_B P_T}{P_B^{\circ}} = 1$$

$$\frac{1}{P_T} = \frac{y_A}{P_A^{\circ}} + \frac{y_B}{P_B^{\circ}}$$

If A is more volatile than B

$$\text{Let } P_A^\circ > P_T > P_B^\circ.$$

$$y_A = \frac{n_A P_A^\circ}{P_T} \quad | \quad y_B = \frac{n_B P_B^\circ}{P_T}$$

$$y_A > n_A$$

$$y_B < n_B$$

\* mol fraction of more volatile substance will be more in vapour phase compared to liquid phase

\* mol fraction of less volatile substance will be more in liquid phase compared to vapour phase

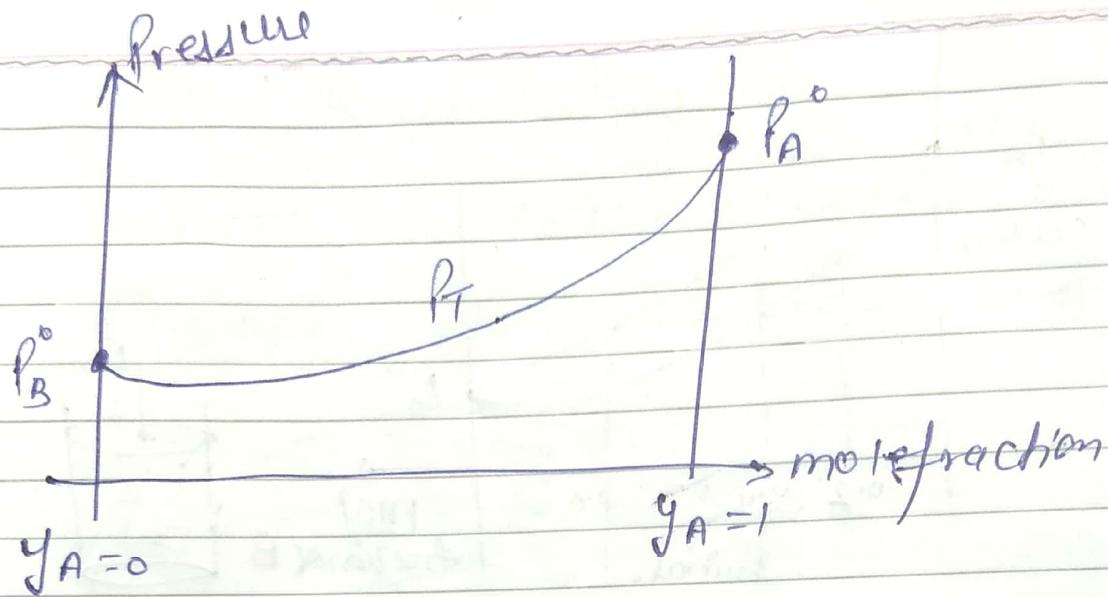
$$\frac{1}{P_T} = \frac{y_A}{P_A^\circ} + \frac{y_B}{P_B^\circ} \quad \left\{ y_A + y_B = 1 \right.$$

$$\frac{1}{P_T} = \frac{y_A}{P_A^\circ} + \frac{1-y_A}{P_B^\circ}$$

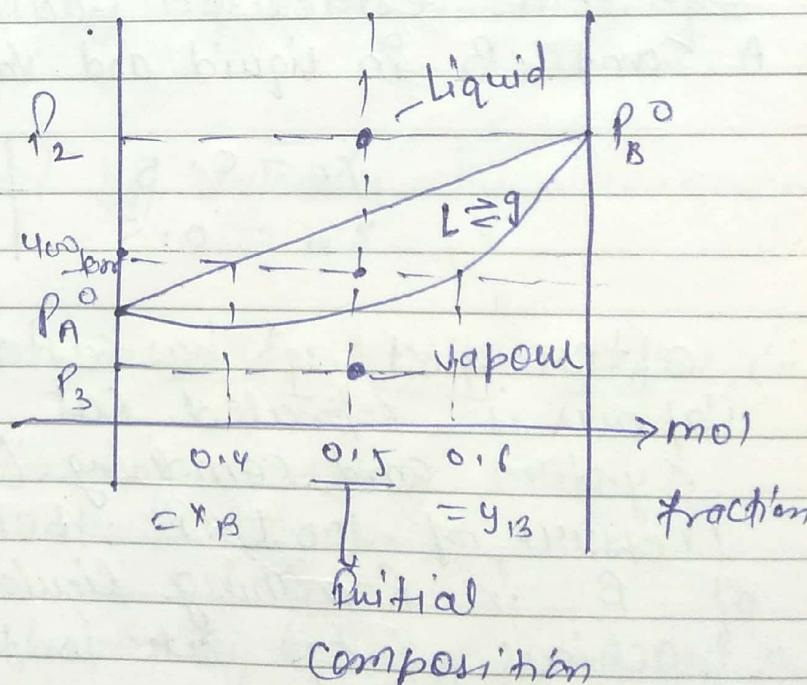
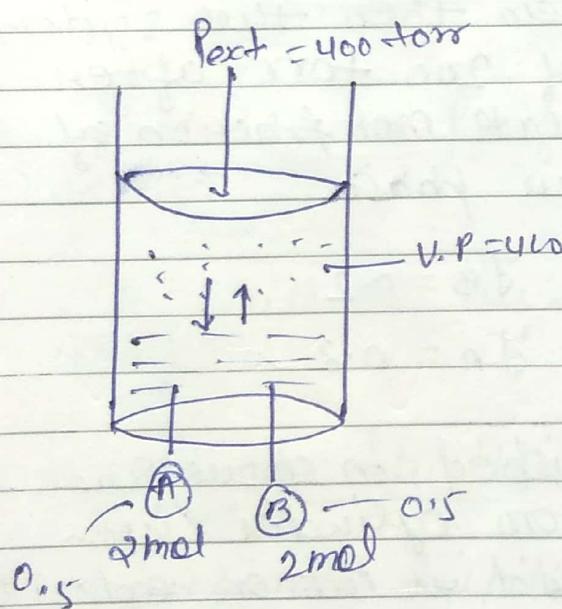
$$\frac{1}{P_T} = y_A \left( \frac{1}{P_A^\circ} - \frac{1}{P_B^\circ} \right) + \frac{1}{P_B^\circ}$$

$$P_T = \frac{1}{y_A \left( \frac{1}{P_A^\circ} - \frac{1}{P_B^\circ} \right) + \frac{1}{P_B^\circ}}$$

$$y = \frac{1}{m_n + c}$$

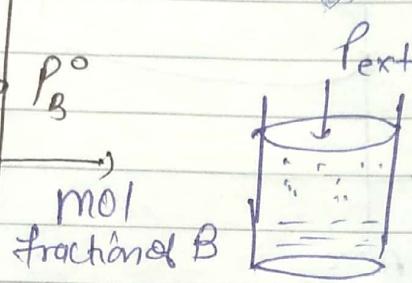
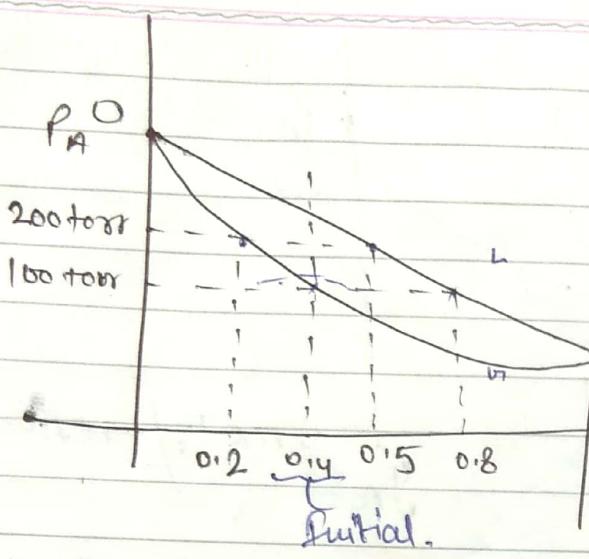


\* fractional distillation:



Ques!

Ques:



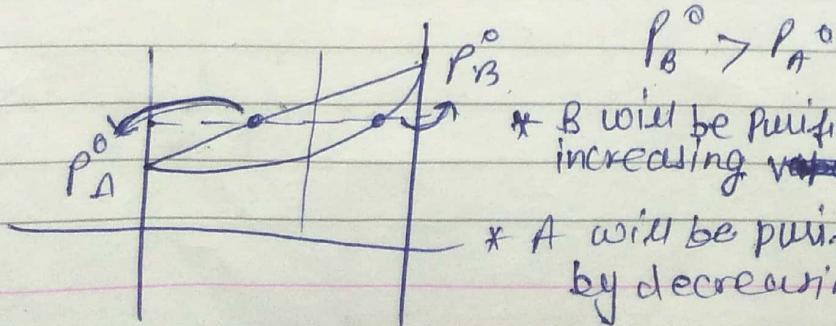
Mole fraction of

Initial 4 mol of B is mixed with 6 mol of A  
in a cylinder piston system then this system  
is put on ext. Pressure of 200 torr after  
eqb has established calculate mole fraction of  
A and B in liquid and vapour phase.

$$\begin{array}{ll} x_B = 0.5 & y_B = 0.2 \\ x_A = 0.5 & y_A = 0.8 \end{array}$$

iii) after first eqb has established in above que  
Vapour is separated out from cylinder piston  
system and remaining liquid is put on ext.  
Pressure of 100 torr then calculate mole fraction  
of B in remaining liquid after this liquid  
achieve eqb at 100 torr.

$$x_B' = 0.8.$$

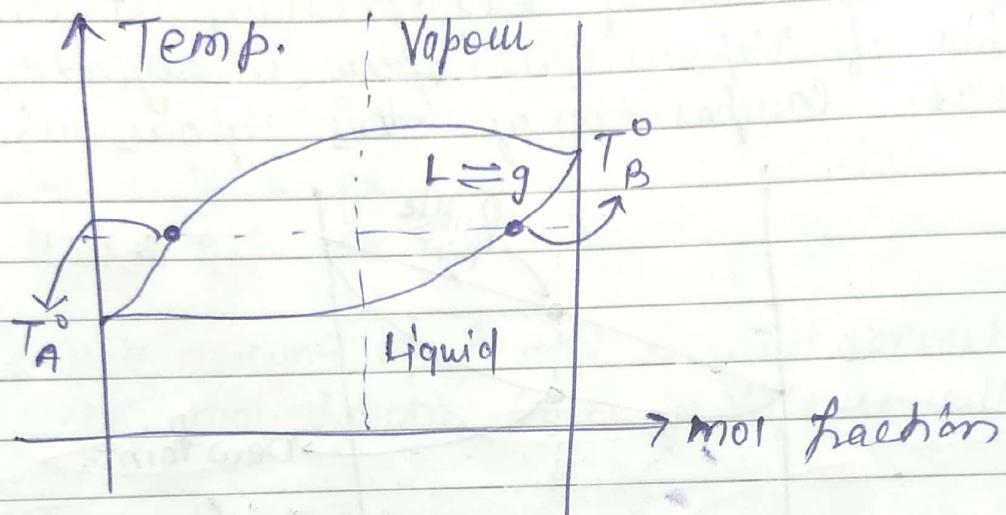


\* B will be purified by vapour by increasing ~~vapour~~ pressure

\* A will be purified by liquid by decreasing pressure.

## Temp. vs mol fraction Curves

$T_A^\circ$  and  $T_B^\circ$  are Boiling point of A and B



- \* B will be purified by liquid by increasing temp.
- \* A will be purified by vapour by decreasing temp.
- \* fractional distillation can be of two type.

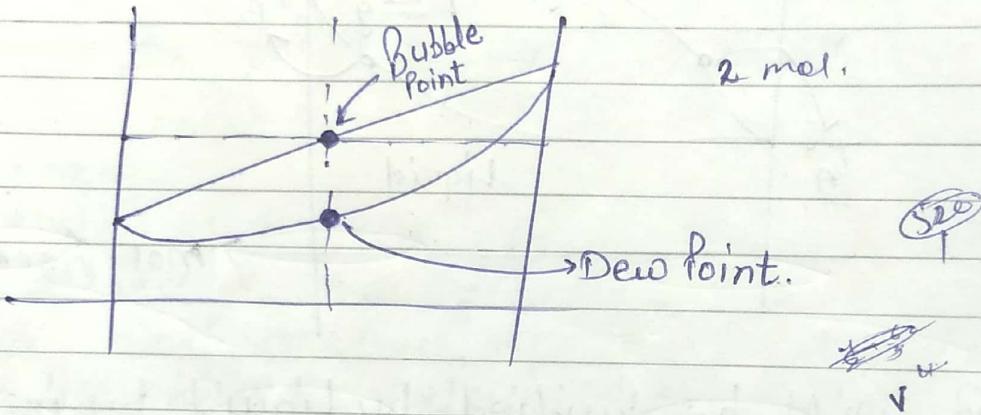
- (i) fractional distillation by Pressure,
- (ii) " " Temp.

Ques. An ideal soln is prepared by mixing 2 mol of A and 3 mol of B. This soln is put under a very high pressure. In a cylinder piston system. Now pressure over the piston increased very gradually then answer the following questions

$$P_A^{\circ} = 400 \text{ torr.}$$

$$P_B^{\circ} = 600 \text{ Torr}$$

(i) Calculate Value of ext. Pressure at which first bubble of vapour will form in cylinder. also calculate composition of this vapour bubble.



$$x_A = \frac{2}{5} \quad x_B = \frac{3}{5}$$

$$P_T = x_A P_A^{\circ} + x_B P_B^{\circ}$$

$$P_T = \frac{2}{5}(400) + \frac{3}{5}(600)$$

$$\underline{P_T = 520 \text{ torr.}}$$

$$y_A = \frac{x_A P_A^{\circ}}{P_T} = \frac{(0.4) \times 400}{520}$$

(iii) Calculate Value of ext. Pressure at which almost complete sol<sup>n</sup> will convert in vapour and last drop of sol<sup>n</sup> remain in liquid form  
 (Dew Point)

$$x_A = \frac{2}{5} \quad y_B = \frac{3}{5}$$

$$\frac{P_f}{P} = x_A P_A^0 + y_B P_B^0$$

$$\frac{1}{P_f} = \frac{y_A}{P_A^0} + \frac{y_B}{P_B^0}$$

Note,

Almost complete amount of A and B will convert in vapour so, mol fraction of A in vapour will be  $\frac{2}{5} = 0.4$ .

$$y_A = \frac{2}{5}, \quad y_B = \frac{3}{5}$$

$$\frac{1}{P_f} = \frac{y_A}{P_A^0} + \frac{y_B}{P_B^0}$$

$$\frac{1}{P_f} = \frac{0.4}{400} + \frac{0.6}{600}$$

$$P_f = 500$$

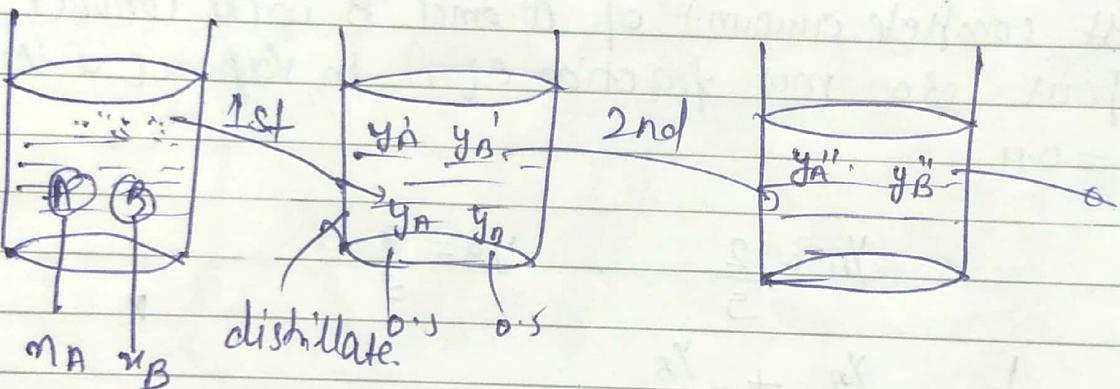
$\Rightarrow$  Composition of last drop of liquid at Dew Point.

$$y_A = \frac{x_A P_A^0}{P_f} \quad 0.4 = \frac{x_A (400)}{500}$$

\* Composition of distillate after an  $n$ -stage of fractional distillation?

\* Condence vapour is called distillate

\* During the Solving Due in liquid sol<sup>n</sup> it is assumed that Vapour is formed in very negligible amount so, Initial composition of liquid can be taken equal to eq<sup>b</sup> composition of liquid.



1st step.

$$y_A = \frac{n_A P_A^0}{P_T} \quad y_B = \frac{n_B P_B^0}{P_T}$$

$$\frac{y_A}{y_B} = \frac{n_A}{n_B} \left( \frac{P_A^0}{P_B^0} \right)$$

2nd step

$$\frac{y'_A}{y'_B} = \frac{y_A}{y_B} \cdot \frac{P_A^0}{P_B^0}$$

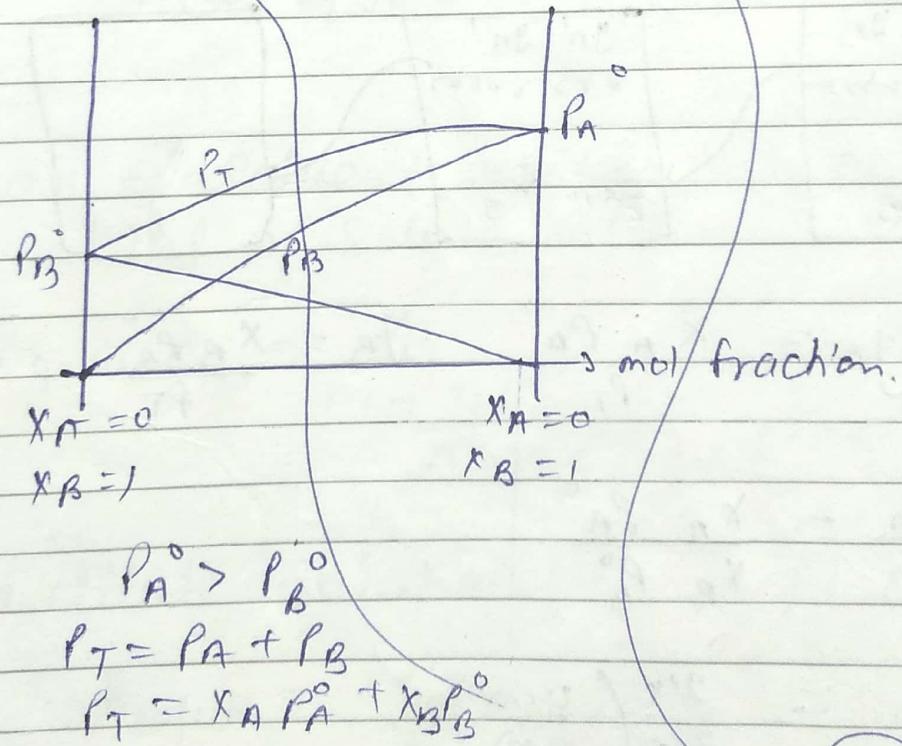
$$\frac{y''_A}{y''_B} = \frac{n_A}{n_B} \left( \frac{P_A^0}{P_B^0} \right)^2$$

after n-step of distillation

$$\left( \frac{y_n}{y_B} \right)_{n\text{-step}} = \frac{x_n}{x_B} \left( \frac{P_A^{\circ}}{P_B^{\circ}} \right)^n$$

Vapour pressure of liquid sol<sup>n</sup> depends on temp. & composition of liquid sol<sup>n</sup>.

Graph (T-constant)



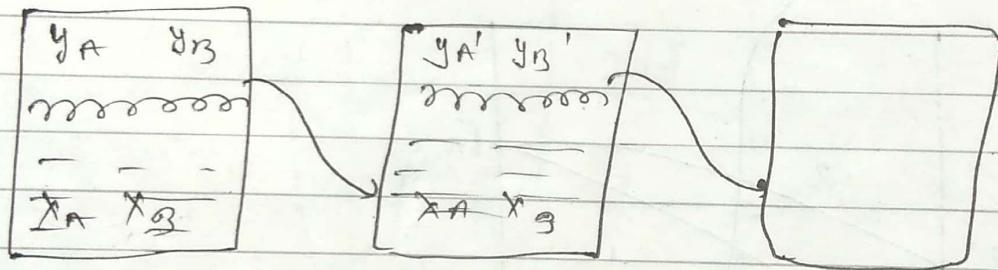
Note: At Boiling Point vapour pressure of liquid will be equal to external pressure & liquid hold e.g. with its vapour

$$P_A^{\circ} > P_B^{\circ}$$
$$T_A^{\circ} > T_B^{\circ}$$

Q. Calculate vapour pressure of 1 molal aq glucose solution if vapour pressure of pure  $\text{H}_2\text{O}$  is 60 torr

$$P_t = X_{\text{H}_2\text{O}} P_{\text{H}_2\text{O}}^0 + X_{\text{glucose}}$$

Q. A solution is prepared by mixing 2 mol. of A & 3 mol of B then calculate vapour pressure of its distillate where  $P_A = 400 \text{ torr}$   
 $P_B = 200 \text{ torr}$



$$y_A = \frac{x_A P_A^0}{P_T} \quad y_B = \frac{x_B P_B^0}{P_T}$$

$$y_A = \frac{x_A P_A^0}{x_B P_B^0}$$

$$\frac{y_A}{1-y_A} = \frac{2/5}{3/5} \left( \frac{400}{200} \right)$$

$$\frac{y_A}{1-y_A} = \frac{4}{3}$$

$$3y_A = 4 - 4y_A$$

$$7y_A = 4$$

$$y_A = 4/7$$

$$y_B = 3/7$$

80

$$P_T' = X_A' P_A^{\circ} + X_B' P_B^{\circ}$$

$$P_T' = \frac{4}{7} \times 400 + \frac{3}{7} \times 200$$

$$P_T' = \frac{2200}{7}$$

\* Relation b/w Mole fraction & Molality:

$$m = \frac{\text{mol of solute}}{\text{mass of solvent in kg}}$$

Let,

$$\begin{aligned} \text{Mass of solvent} &= 1 \text{ kg} = 1000 \text{ gm} \\ \text{mol of Solute} &= m \end{aligned}$$

$$X_{\text{solute}} = \frac{m}{m + 1000}$$

Mol (Solute)

for a dilute solution:

$$X_{\text{solute}} = \frac{m}{1000}$$

Mol (Solute)

\* Relation b/w Molality & molality:

$$m = \frac{\text{mol of solute}}{\text{mass of solvent in kg.}}$$

Let, mass of solvent in 1 kg = 1000 gm  
mol Solute = m mol.

$$M = \frac{m}{\frac{1000 + m(\text{mwf solute})}{1000 d_{\text{sol}}}}$$

when  
 $c_{\text{sol}} = \text{gm/ml.}$

For dilute solution:

$$M = \frac{m}{\frac{1000 + m(\text{mwf})}{1000 d_{\text{sol}}}}$$

$$M = m d_{\text{sol}}$$

For dilute aq. Solution:  $c_{\text{sol}} \approx \text{gm/ml}$

$$\boxed{M \approx m}$$

D.M.P.

\* Colligative Properties:

for the definite amount of a definite solvent properties that depend on No. of Solute Particles Called Colligative Properties

Colligative Property do not depend on nature of Solute because during the study of Colligative Properties always use a Non-volatile solute.

\* Colligative Properties can be of 4 types:

- (1) Lowering in V.P or relative lowering in V.P
- (2) Elevation in Boiling point
- (3) Preparation in freezing Point.
- (4) Osmotic Pressure

### (1) Lowering Or Relative lowering in V.P

If a non-volatile solute is mixed in a solvent than vapour pressure of resulting solution will be less than vapour pressure of pure solvent. This is called Lowering in vapour pressure.  $\text{Solvent} + \text{Solute} = \text{Sol}^n$

$$P_T > P_0$$

$$P_T = X_{\text{solvent}} \cdot P^{\circ}_{\text{solvent}} + X_{\text{solute}} \cdot P^{\circ}_{\text{solute}}$$

$$P_T = X_{\text{solvent}} + P^{\circ}$$

$$P_T \cancel{=} P^{\circ} \Rightarrow \Delta P = P^{\circ} - P_T$$

$$\Delta P = P^{\circ} - P_T$$

$$\Delta P = P^{\circ} (1 - X_{\text{solvent}})$$

$$\Delta P = X_{\text{solvent}} P^{\circ}$$

relative lowering in v.p.

$$\frac{\Delta P}{P^{\circ}} = \chi_{\text{solute}}$$

$$\frac{P_T - P^{\circ}}{P^{\circ}} = \frac{n}{n+N}$$

for dilute solution :  $N \ggg n$ .

$$\frac{P^{\circ} - P_T}{P^{\circ}} = \frac{n}{N}$$

$$\chi_{\text{solute}} = \frac{n}{n+N}$$

where  $n = \text{mol of solute}$   
 $n = \text{mol of solvent}$

For any solution :

$$\frac{P^{\circ} - P_T}{P^{\circ}} = \frac{n}{N+n}$$

$$\frac{a}{b} = \frac{x}{y}$$

$$\frac{a}{b-a} = \frac{x}{y-x}$$

Q. A  $373^{\circ}\text{K}$  K(100°C) Relative lowering in v.p. of aq. glucose soln is 10%. than calculate molality of glucose in soln & also calculate v.p. of soln.

Sol: Boiling Point of  $\text{H}_2\text{O} = 373^{\circ}\text{K}$

$$S^{\circ}, P_{\text{H}_2\text{O}} = 1 \text{ atm} = 768 \text{ Torr}$$

$$\frac{\Delta P}{P^{\circ}} * 100 = 10 \text{ so } \frac{\Delta P}{P^{\circ}} = \frac{1}{10}$$

$$\phi_0 \cdot X_{\text{solute}} = 0.1 = \frac{n_{\text{solute}}}{n_{\text{solute}} + n_{\text{solvent}}}$$

$$n_{\text{solute}} + n_{\text{solvent}} = 1$$

$$\Rightarrow n_{\text{solute}} = 0.1$$

$$\phi_0, m = \frac{0.1}{0.9 \times 18} = \frac{1000}{9 \times 18}$$

$$\text{we know that: } \frac{\rho - \rho_0}{\rho_0} = 0.1$$

$$\therefore \frac{P^0 - P_T}{P^0} = 0.1 \quad \frac{760 - P_T}{760} = 0.1$$

$$P_T = 684$$

## 2) Elevation in Boiling Point: ( $\Delta T_b$ )

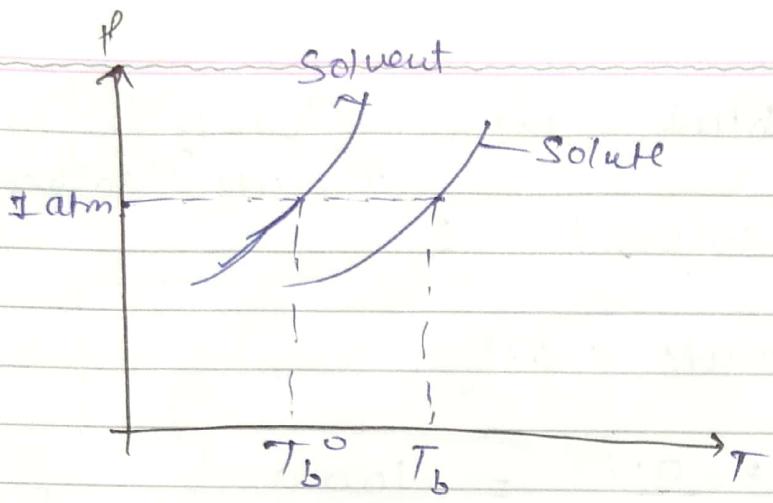
On mixing Non-Volatile Solute in Solvent B.P. of resulting soln will be more or less compared to pure solvent it is called elevation in Boiling Point

Solvent + non-volatile solute = soln

$$T_b^0 < T_b$$

$$\Delta T_b = T_b - T_b^0$$

Elevation in B.P.,



$$\Delta T_b \propto \Delta P \propto \frac{1}{x_{\text{atm}}} \propto m$$

$$\Delta T_b \propto m$$

$$\boxed{\Delta T_b = k_b m}$$

Here  $k_b$  called Mole elevation  
constant or ebullioscopic const

$$\boxed{k_b = \frac{R(T_b^o)^2 \cdot M_w \text{ (solvent)}}{1000 \times \Delta H_{\text{vap}}}}$$

$k_b$  depend on solvent

\* Important Point

\* Value of  $k_b$  depend on Nature of solvent  
 \* At Boiling Point in such soln in which  
 Non-volatile solute is present liquid  
 solvent will be in eqb. with vapour

### (3) Depression in Freezing point:

on mixing Non-Volatile Solute in Solvent Freezing Point of Resultant soln will be less than freezing Point of Pure solvent this is called depression in freezing point.

Solvent + non-volatile solute = Solution.

$T_f^\circ$

$$\Delta T_f^\circ = T_f^\circ - T_f$$

$$\Delta T_f \propto \Delta T_b \propto \Delta P \propto X_{\text{dilute}} \propto m.$$

$$\Delta T_f \propto m$$

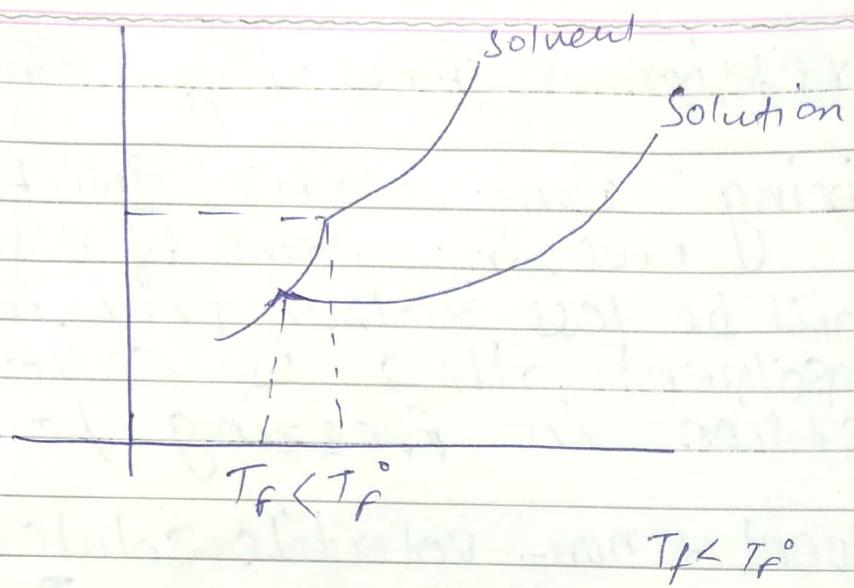
$$\Delta T_f \propto m$$

$$\Delta T_f = k_f m$$

Here,  $k_f$  is called molal depression constant or cryoscopic constant.

$$k_f = \frac{R(T_f^\circ)}{1000 \times \Delta H_{\text{fusion}}} \text{ M.wt (solvent)}$$

$k_f$  depend on solvent



⇒ In Colligative Property depression in freezing point -  
Liquid solvent will be in eq<sup>b</sup>. with Solid Solvent

Q. % lowering in vapour pressure of  $\text{urea}$  is  
1% then calculate freezing point of this sol.

$$K_f \text{ for } \text{H}_2\text{O} = 1.8 \text{ K} \cdot \text{kg mol}^{-1}$$

$$\left( \frac{\Delta P}{P_0} \right) \times 100 = 1 \quad \text{NH}_2\text{CONH}_2 \\ \text{Molar mass} = 60 \text{ gm/mol}$$

$$X_{\text{urea}} = \frac{1}{100}$$

Solute =  
 $\text{NH}_2\text{CONH}_2$

$$\Delta T_f = K_f m$$

$$X_{\text{urea}} = \frac{1}{100} = \frac{n_{\text{urea}}}{n_{\text{urea}} + n_{\text{H}_2\text{O}}}$$

$$n_{\text{urea}} + n_{\text{H}_2\text{O}} = 1 \text{ mol.}$$

$$n_{\text{urea}} = 0.01 \text{ mol.}$$

$$n_{\text{H}_2\text{O}} \approx 1 \text{ mol}$$

$$m = \frac{0.01}{\frac{1 \times 18}{1000}} = \frac{10}{18}$$

$\Delta T_f = k_f m$

$$\Delta T_f = (1.8) \left( \frac{1}{18} \right) = 1$$

$$T_f = -1^\circ\text{C} \text{ or } 272 \text{ Kelvin.}$$

Q. 8 gram Urea is mixed in 100 ml of Pure  $\text{H}_2\text{O}$  resultant solution is put at  $-9^\circ\text{C}$  then calculate amount of ice that can be separated out.

$$K_f = 1.8 \text{ K. kg. mol}^{-1}$$

$$K_f = 1.8 \text{ K. kg.}$$

$$= -9^\circ\text{C}$$

$$= -9$$

1 mol of solute  
 160 g  
 mass of solvent 18 g  
 $0.2 \text{ mol} \cdot \frac{18 \text{ g}}{160 \text{ g}}$   
 mass of  
 solvent 1.6 g

$$K_f = \frac{1}{I} =$$

$$= 9$$

$$\text{mass of solvent in 100 g} = \frac{1.6}{60} \text{ kg.}$$

$$= \frac{1600}{60} = \frac{160}{6} = 26.67 \text{ g}$$

$$= 100 - 26.67 = 73.33$$

(ii) For above case if initial solution is put on ext. temp. of  $105^{\circ}\text{C}$  then calculate mass of  $\text{H}_2\text{O}$  that can be separated as vapour.

$\Rightarrow$

$$K_b = 0.5 \text{ K kg mol}^{-1}$$

100

$$\eta = \frac{m}{m_{\text{sol}}} \cdot$$

$$\Delta T_b = K_b \frac{\text{mol of solute}}{\text{mass of solvent in kg}}$$

$105 -$

$$5 = 0.5 \text{ K} \frac{(8/60)}{\text{mass of solvent in kg}}$$

$$\text{mass of solvent} = \frac{0.8}{60} \text{ kg}$$

$$= \frac{80}{60} =$$

$$= 100 - \frac{80}{6}$$

Boiling point, freezing pt. is automatically equal to surrounding temp.

b. for a sol<sup>n</sup> during a colligative property

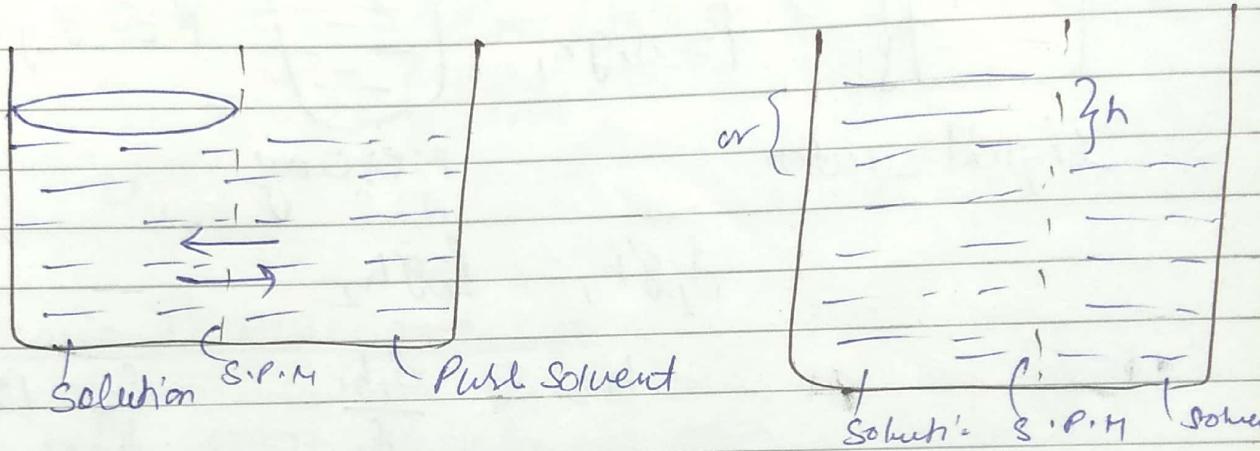
\* Osmotic Pressure ( $\Pi$ ) ?

\* Osmotic: flow of solvent particles from pure solvent to solution through S.P.M (semi-permeable membrane). Called osmotic.

$$N_{\text{w}} = 16 - 26 - J(A) \\ + \\ \boxed{1 \text{ to } 10 \text{ S-1}}$$

### \* Osmotic pressure :-

Ext. Pressure applied over sol<sup>u</sup> or hydrostatic pressure develop over the solution to stop osmotic called osmotic pressure.



$$\Pi = C S T$$

$$\Pi = S g h$$

$$\boxed{\Pi = C S T = S g h}$$

$$\boxed{S = 0.0821}$$

$$S = \text{solution constant} = 0.0821 \frac{\text{atm} \cdot \text{lit}}{\text{mol} \cdot \text{ic.}}$$

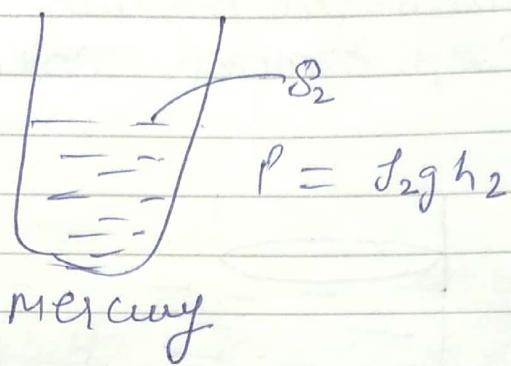
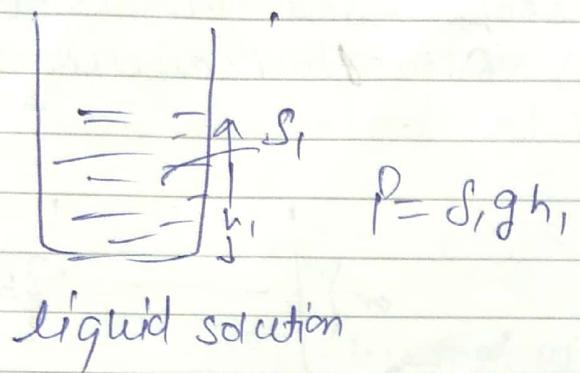
### \* Reverse osmosis :-

Applied ext. pressure over solution is more then osmotic pressure then flow of solvent particles is start from solution to pure solvent this is called reverse osmosis.

Reverse osmotic can be used for desalination of impure water.

$$[760 \text{ mm of Hg} = 1 \text{ atm}]$$

\* Calculation of Sgh by mercury scale Calibration.



$$\rho_1 gh_1 = \rho_2 gh_2$$

$$h_2 = \frac{\rho_1 h_1}{\rho_2}$$

$\rho_2 = 13.6 \text{ gm/ml.}$   
Density of  
mercury.

$\Rightarrow \Pi_1 = \Pi_2$  (Isotonic solution)

$\Pi_1 > \Pi_2$   $\Pi_1$  is hypertonic then  $\Pi_2$

$\Pi_1 < \Pi_2$   $\Pi_1$  is hypotonic then  $\Pi_2$

Ques: 0.2 Molar glucose solution is Isotonic with 5% w/v soln of a non-volatile substance at same temp. Then calculate molecular wt. of non-volatile substance.

$$\frac{W_{\text{solute}}}{V_{\text{solution}}} \times 100 = 5$$

me. let,  $V_{\text{solution}} = 100 \text{ ml.}$

$$W_{\text{solute}} = 5 \text{ gm.}$$

$$M = \frac{(\gamma \cdot w/v) / m \cdot wt \text{ (solute)}}{(100/1000)}$$

$$\boxed{\text{Molarity} = \frac{\gamma \cdot w/v \times 10}{m \cdot wt \text{ (solute)}}}$$

$$C_1 RT = C_2 RT$$

$$0.2 = \frac{5/m \cdot wt \text{ (solute)}}{\left(\frac{100}{1000}\right)}$$

$$M \cdot wt = 250.$$

Q. Osmotic pressure ~~rise~~ in 0.001  $\text{w/v}$  soln of a non-volatile substance is 13.6 mm. Then calculate m.wt of non-volatile substance

$$\text{Temp} = 300\text{K}$$

$$\text{density of solution} = 0.76 \text{ gm/ml.}$$

extra height 13.6 mm.

$$\Pi = cst$$

$$\Pi = \rho gh$$

$$\frac{\gamma \cdot w}{v}$$

$$= \frac{w_{\text{solute}} \times 100}{V_{\text{solution}}} = 0.001.$$

$$\text{Let } V_{\text{solution}} = 100$$

$$w_{\text{solute}} = 0.001$$

$$S_1 h_1 = S_2 h_2$$

$$h_2 = \frac{S_1 h_1}{S_2}$$

$$= \frac{(0.76)(13.6)}{13.6} = 0.76 \text{ mm of Hg.}$$

$$\text{Molarity} = \frac{\gamma \cdot w/v \times 10}{m \cdot wt \text{ (solute)}}$$

$$\text{Osmotic Pressure} = \frac{0.76}{760} = 10^{-3} \text{ atm.}$$

$$\Pi = cst$$

$$\text{arrow} = i \text{ mol/l}$$

$$10^{-3} = \frac{0.001 \times 10}{\text{M.wt}} \times 0.0821 \times 300$$

~~Abnormal~~

~~Abnormal~~  
~~factor~~

Abnormal Colligative Properties and  
van't Hoff factor (i):

If Solute particles associate or dissociate then actual value (Practical value or observed value) of colligative property will be different from theoretical value (expected value) of colligative property.

This is called abnormal colligative property and can be represented by van't Hoff factor  $i$ .

$i = \frac{\text{final mol. of solute in solution}}{\text{initial mol. of solute in soln}} = \frac{\text{observed value of c.p.}}{\text{theoretical value of c.p.}}$

$= \frac{\text{Theoretical molar mass of solute}}{\text{Observed molar mass of solute}}$

$$\Delta T_b = K_b (i m)$$

$$\Delta T_f = K_f (i m)$$

$$\Pi = i c R T$$

$$\frac{\Delta P}{P^0} = \frac{i n}{i n + N}$$

for dilute solution  $N \gg \gg n$

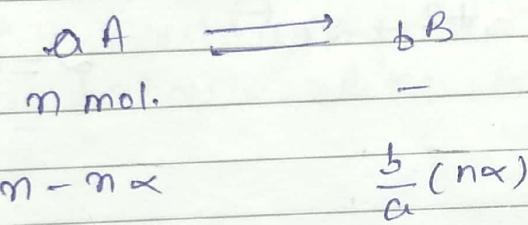
$$\frac{\Delta P}{P^0} = \frac{i n}{N}$$

If more than one type of solute are present in solution then

$$\pi = (i_1 c_1 + i_2 c_2 + i_3 c_3 + \dots) RT$$

$$\Delta T_b = K_b (i_{1m_1} + i_{2m_2} + i_{3m_3} + \dots)$$

\* Relation b/w Van't Hoff factor  $i$  and  $\alpha$  (degree of dissociation)



$$n_{\text{initial}} = n$$

$$n_{\text{observed}} = n - n\alpha + \frac{b}{a}(n\alpha)$$

$$i = \frac{n_{\text{observed}}}{n_{\text{initial}}} = \frac{n - n\alpha + \frac{b}{a}(n\alpha)}{n}$$

$$= \frac{M_{\text{Theoretical}}}{M_{\text{observed}}}$$

$$i = 1 - \alpha + \frac{b}{a}\alpha$$

$$i = 1 + \left(\frac{b}{a} - 1\right)\alpha$$

$$i = 1 + (n-1)\alpha$$

$$n = \frac{\text{s.c. of Product}}{\text{s.c. of Reactants}}$$

$$i = 1 - \alpha + n\alpha$$

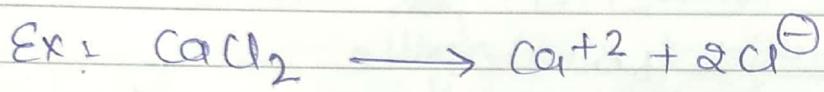
Calculation of  $i^{\circ}$  for different type of substance:

i) for non-electrolyte?

for ex: urea, glucose, fructose etc.

$$\alpha = 0 \quad i^{\circ} = 1$$

ii) for strong electrolytes?

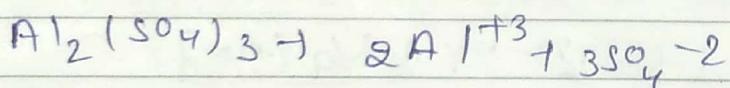


$$\alpha = 1$$

$$i^{\circ} = 1 + \left(\frac{3}{1} - 1\right)(1)$$

$$i^{\circ} = 3$$

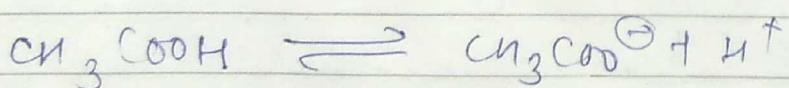
for strong electrolytes value of van't Hoff factor will be equal to no. of mol. of ions provided by one mol. electrolyte.



$$i^{\circ} = 1 + (5 - 1)(1) \quad \alpha = 1$$

$$i^{\circ} = 5$$

iii) In Partial dissociate or weak electrolyte!



$$\alpha < 1$$

$$i^{\circ} = 1 + (2 - 1)\alpha$$

$$i^{\circ} = 1 + \alpha$$

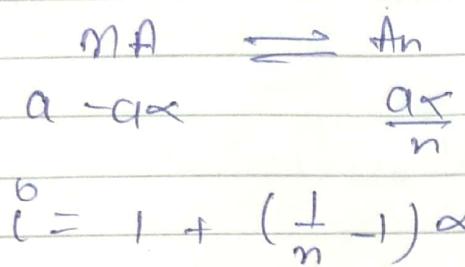
$$An = nA$$

$$i^{\circ} = 1 + (n-1)\alpha$$

L.S = 5- 11 to 25

E.C J.A = 26 to 30  
ZP

## \* In dilute association Rxn:



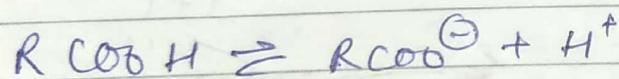
$$\bar{f}^o = 1 - \alpha + \frac{\alpha}{n}$$

Here  $\alpha$  will be degree of association.

Note: for carboxylic acids in their aq. sol<sup>n</sup> they behave like weak electrolyte.

in e

In aqueous sol<sup>n</sup>



$$\bar{f}^o = 1 + (2-1)\alpha$$

$$\bar{f} = 1 + \alpha$$

In benzene



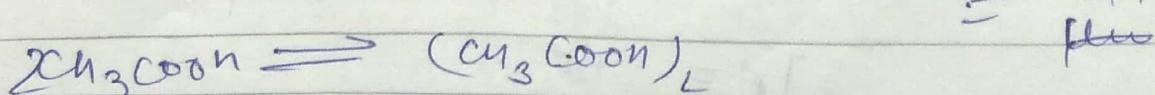
$$\bar{f}^o = 1 + \left( \frac{1}{2} - 1 \right) \alpha$$

$$\bar{f} = 1 - \frac{\alpha}{2}$$

\* Unknown solutes are considered non-electrolytes.

Ques: degree of dissociation of acetic acid in Benzene is 40%. then calculate observed molar mass of acetic acid in Benzene

Ans:



$$i = 1 + \left(\frac{1}{2} - 1\right) \alpha = \frac{n_{\text{observed}}}{n_{\text{theoretical}}} \cdot \frac{M_{\text{theoretical}}}{M_{\text{obs.}}}$$

$$\therefore 1 + \left(\frac{1}{2} - 1\right) (0.4) = \frac{60}{M_{\text{obs.}}}$$

Ques: Calculate Normal freezing point of 3.68% w/w  
aq. soln of  $\text{K}_4[\text{Fe}(\text{CN})_6]$   $M_{\text{wt}} = 368$ .

$$K_f(\text{H}_2\text{O}) = 1.9284 \text{ K} \cdot \text{kg/mol}$$

$$\frac{1.9284}{0.9632} = 2.$$

$$\stackrel{0}{U} = 5.$$

$$\Delta T_f = K_f (i_m)$$

$$\Delta T_f =$$

Molality = mole of solute

$$\frac{\omega_{\text{solute}}}{\omega_{\text{solution}}} \times 100 = 3.68$$

let  $\omega_{\text{solution}} = 100$

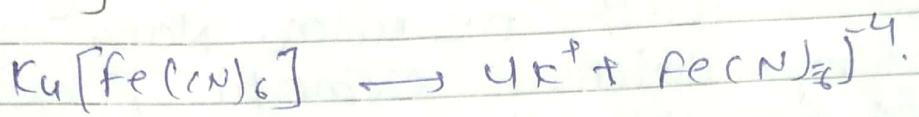
$$\omega_{\text{solute}} = 3.68$$

$$\Delta T_f = (1.9284)(5) \cdot \frac{\left(\frac{3.68}{368}\right)}{\left(\frac{96.32}{100}\right)}$$

$$\Delta T_f = 1$$

$$T_f = -1^\circ\text{C}$$

Ques: In above Ques. if observed value of freezing point is  $-0.5^{\circ}\text{C}$  then calculate degree of dissociation of  $\text{K}_4[\text{Fe}(\text{CN})_6]$ .  $\Delta T_f = -0.5^{\circ}\text{C}$ .



$i = 0.5$

(1)

$$0.5 = (1.4284)(i) \frac{(3.68/368)}{\left(\frac{96.32}{1000}\right)}$$

$$i = 2.5$$

$$i = 1 + \left(\frac{5}{1} - 1\right)\alpha$$

$$2.5 = 1 + 4\alpha$$

$$\alpha = \frac{3}{8} = 0.375$$

$= 1 + 1.25$

Q. 100ml 1Molar NaCl is mixed with 50ml, 0.5 M KCl soln. at 300K. Then calculate osmotic pressure of resultant 0.01M soln.

(2)

$T =$

$$\Pi = CRT$$

$$\begin{aligned} \Pi &= (i_1 C_1 + i_2 C_2) RT \\ &= (2 \times 1 + 2 \times 1)(0.0821)(300) X \end{aligned}$$

$$\begin{aligned} i &= 1 + 2 \\ i &= 3 \end{aligned}$$

$$\Rightarrow [\text{NaCl}]_{\text{Resultant}} = \frac{1 \times 100}{180} = \frac{10}{15}$$

$$[\text{KCl}]_{\text{Res.}} = \frac{0.5 \times 50}{150} = \frac{1}{6}$$

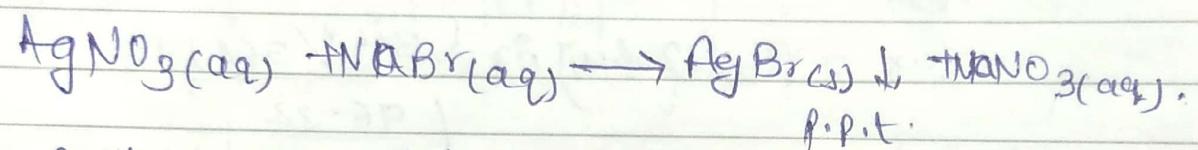
$$\Pi = \left( 2 \times \frac{10}{15} + 2 \times \frac{1}{6} \right) (0.0821)(300)$$

Q. Equal Volume of 0.4 Molar  $\text{AgNO}_3(\text{aq})$  is mixed with 0.2 Molar  $\text{NaBr}(\text{aq})$  at 300 K temp. Calculate osmotic pressure of resultant soln.

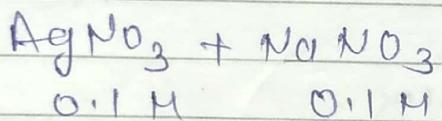
$$\Pi = CRT$$

$$= \boxed{0.2}$$

$$=$$



0.2 M	0.1	X	
0.1 M	-	0.1 M	0.1 M



$$\Pi = (i_1 c_1 + i_2 c_2) RT$$

$$= (2 \times 0.1 + 2 \times 0.1)(0.0821)(300).$$

\* Solubility of gas in liquid solution:

i) factors Affecting Solubility of gas in liquid soln:

ii) Nature of gas:

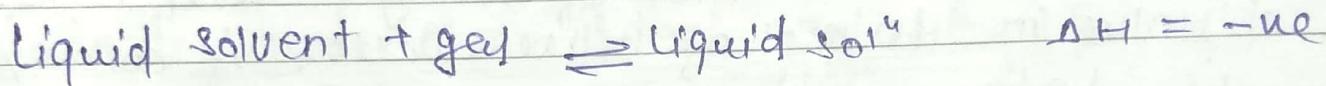
Polar gases dissolve more in polar solvent and non-Polar dissolve more in non-polar solvent.

iii) Pressure:

On increasing Pressure solubility of gases increases

iii) Temperature:

on increasing temp. solubility of gases decrease.



\* Henry's law for solubility of gases:

Mol. fraction of gas in liquid solution will be proportional to Partial Pressure of gas over the solution

$$P_A \propto x_A$$

$$P_A = K_H x_A$$

$K_H$  ↑ soln.

$K_H$  ⇒ Henry's constant.

if value of  $K_H$  is high then solubility of gas in solution will be less.

Q. Compare the value of  $K_H$  for  $N_2$  and  $NH_3$  in  $H_2O$

$$K_{H(NH_3)} < K_{H(N_2)}$$

\* Value of Henry const.  $k_H$  depend on nature of gas, nature of solvent and temperature.

On increasing temp. ~~value~~ value of  $k_H$  increase.

Ques: In atmosphere mol. fraction of Nitrogen is 0.8 then calculate mol. of Nitrogen that will dissolve in 10 mol of pure water if atmospheric is 1 atm.

$$K_H(N_2) = 10^5 \text{ atm.}$$

$$P_{N_2} = 0.8 \times 1 \\ = 0.8 \text{ atm.}$$

$$P_{N_2} = K_H \times N_2.$$

$$0.8 = 10^5 \times \left( \frac{n_{N_2}}{n_{H_2} + 10} \right)$$

$$8 \times 10^{-6} = \frac{n_{N_2}}{n_{H_2} + 10}$$

$$8 \times 10^{-5} + (8 \times 10^{-6}) n_{N_2} = n_{H_2}$$

$$8 \times 10^{-5} = n_{N_2} (1 - 8 \times 10^{-6})$$

$$n_{N_2} = 8 \times 10^{-5}$$

Ques: In a close cylinder piston system over benzene two gases are present in 3:4 mol ratio if total gaseous pressure over the benzene is 5 atm. then calculate solubility of gas A in benzene in mol/litre.

$$d_{benzene} = 0.89 \text{ g/ml}$$

$$k_H \text{ for A in benzene} = 10^4 \text{ atm.}$$

Suppose B is insoluble.

$$P_A = \frac{5}{7} \times 3.$$

- Every else

v.p. vapour pressure

φ

$$\bar{P}_n = k_B \times n.$$

$$\frac{5}{7} \times 3 =$$

$$P_A = k_B \cdot \bar{x}_n$$

$$= \frac{15}{7} = 10^4$$

$$\frac{5}{7} \times 3 = 10^4 \left( \frac{n_A}{m_A + \frac{800}{7B}} \right)$$

solvent = 1 L.

mass of C<sub>6</sub>H<sub>6</sub> = 800 g.

## \* Ideal and non-Ideal solution's:

Ideal solution

+ve deviated ideal  
solution

-ve deviated ideal  
solution

x) if follow Raoult's law

⇒ Do not follow  
Raoult's law ~~actual~~  
V.P of sol<sup>n</sup> will be  
more than calculated  
from Raoult's law

⇒ Do not follow  
Raoult's law ~~actual~~  
V.P of sol<sup>n</sup> will be  
less than calculated  
from Raoult's law.

$$P_A = n_A P_A^0$$

$$P_B = n_B P_B^0$$

$$P_A > n_A P_A^0$$

$$P_B > n_B P_B^0$$

$$P_A < n_A P_A^0$$

$$P_B < n_B P_B^0$$

2) Bond strength  
b/w solute and  
solvent will be  
almost equal to  
bond strength in  
pure solvent and  
in pure solute.

$$\Delta H_{mix} = 0$$

$$\Delta V_{mix} = 0$$

⇒ In sol<sup>n</sup> Bond st. b/w  
solute and solvent  
will be less as comp-  
ared to bond st.  
in solute and solvent  
when they are  
separated.

$$\Delta H_{mix} > 0$$

$$\Delta V_{mix} > 0$$

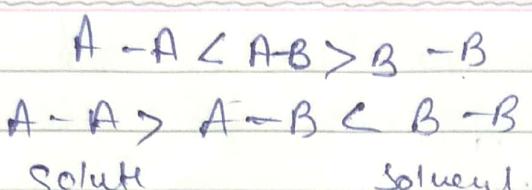
$$\Delta H_{mix} < 0 \quad \left. \begin{array}{l} \text{Bond} \\ \text{strength} \end{array} \right\}$$

$$\Delta V_{mix} < 0$$

Solid state  
thermodynamics.  
Liquid soln.

(i) kinetics  
radioactive  
(ii) chemical equilibrium  
Redox,  
Electrochemistry -  
(iii) Ionic Equilibrium, (conductance)

+ve  
-ve



$$\Delta S_{\text{univ}} = -\frac{q_{\text{sys}}}{T}$$

Polar.

+ve

-ve

$$\Delta S_{\text{mix}} > 0$$

$$\Delta S_{\text{mix}} > 0$$

$$\Delta S_{\text{mix}} > 0$$

$$\Delta H_{\text{mix}} < 0$$

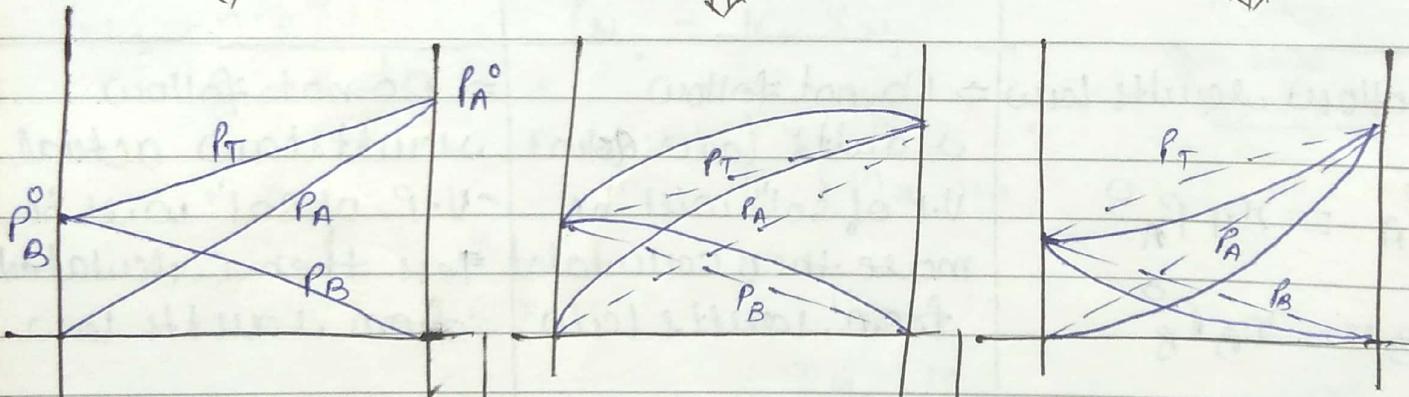
$$\Delta H_{\text{mix}} < 0$$

$$\Delta H_{\text{mix}} < 0$$

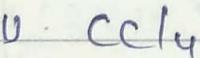
$$\Delta S_{\text{univ.}} = -\frac{q_{\text{sys}}}{T} = 0$$

$$\Delta G_{\text{univ.}} = -\frac{q_{\text{sys}}}{T} < 0$$

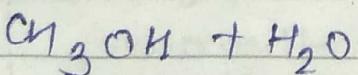
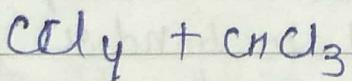
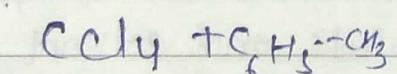
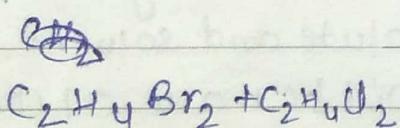
$$\Delta S_{\text{univ.}} = -\frac{q_{\text{sys}}}{T} > 0$$



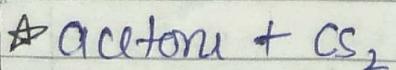
$\Rightarrow$  similar structures



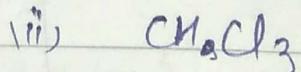
EA!



\* benzene + toluene

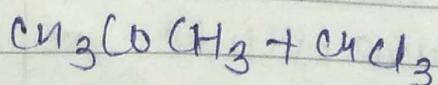
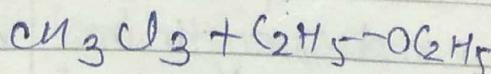


(i) acid / base



EA!

Acetone + aniline  
HCl + water



characteristics 1 gm & 4  
per gram  
800000  $\frac{100}{50} = 2$

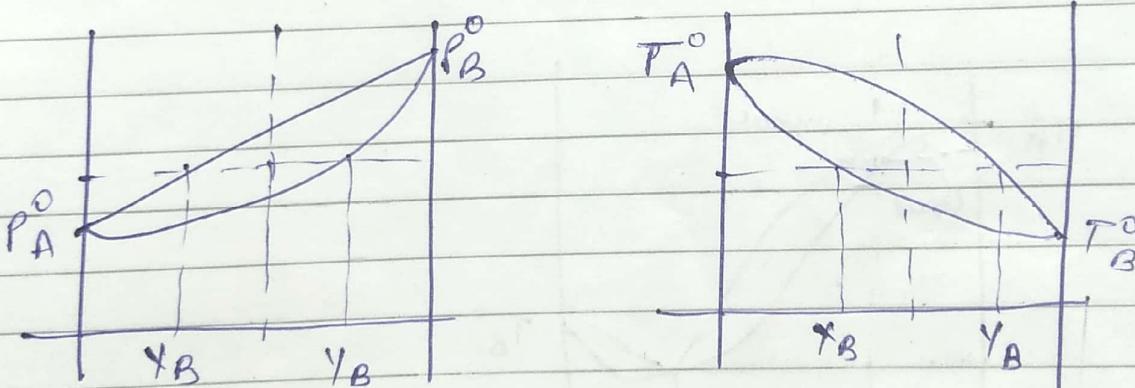
L.SHD  $\rightarrow 1 \Rightarrow 1 + 10^{14}$   
 $\infty \Rightarrow 5A \Rightarrow 31 + 35$

### \* Azeotrope solution:

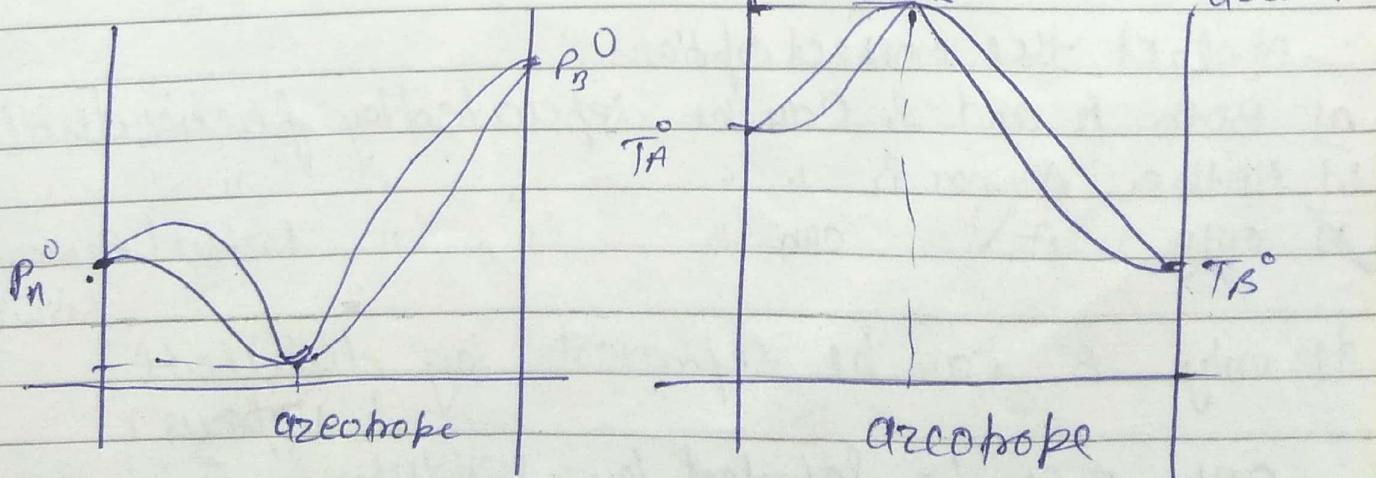
Azeotrope solution which have equal mol fraction in liquid phase and vapour phase called azeotrope solution

\* Azeotrope sol<sup>ly</sup> can not be purified with the help of fractional distillation.

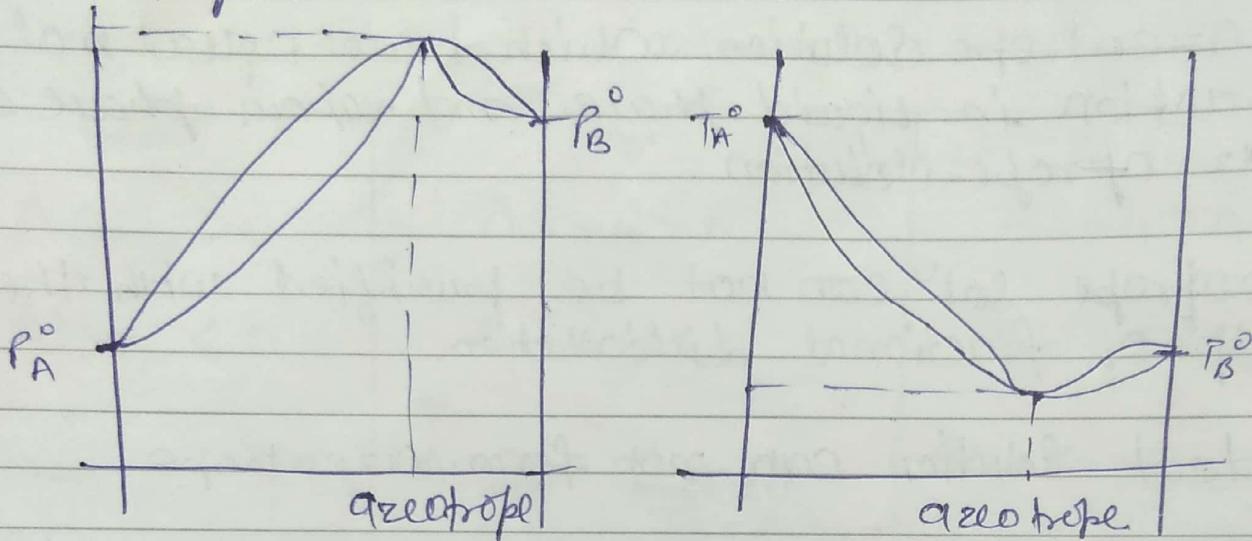
\* Ideal solution can not form azeotrope



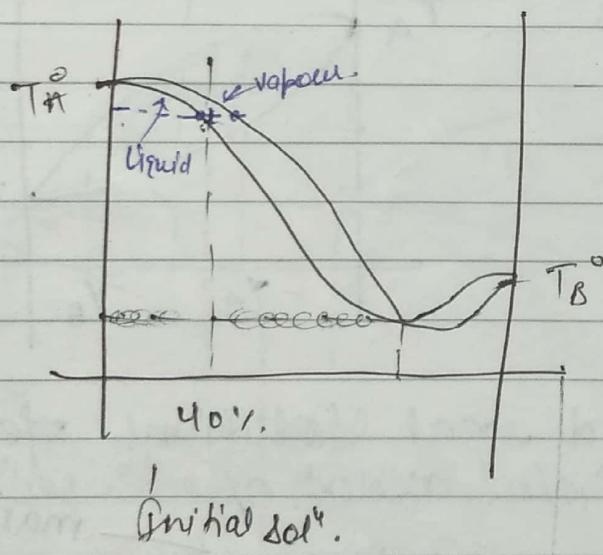
\* Negatively deviated real solutions form maximum boiling point azeotrope



\* Positively deviated real solution form minimum azeotrope.



Ques!



Initial sol<sup>n</sup>.

Select the correct options

- a) Both A and B can be separated by fractional distillation.
- b) Neither A nor B " "
- c) only A can " " Residue (Remaining liquid)
- d) only B can be separated by distillate (Vapours)
- e) only A can be separated by residue